

Effective Algebraic Analysis in Linear Control Theory

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Summary by Frédéric Chyzak

Abstract

In the 1960's, Malgrange made use of D-module theory for studying linear systems of PDEs [2]. Several aspects of this approach, now called *algebraic analysis*, have then been made effective in the 1990's, owing to the extension of the theory of Gröbner bases to rings of differential operators. Correspondingly, algorithms have also been implemented in several systems. Recently, the introduction of algebraic analysis to control theory has allowed to classify linear multidimensional control systems according to algebraic properties of associated D-modules, to redefine their structural properties in a more intrinsic fashion, and to develop effective tests for deciding these structural properties [3, 6, 7, 8, 9, 10, 12, 14].

1. From Linear Multidimensional Control Systems to Algebraic Analysis

A control system relates the state x of a physical process with an external command u and some output y . Each of u , x , and y is a vector of functions of the time t , and the system describes their evolution with t . Several classes of such systems can be represented by matrices with coefficients in a ring of operators. Sample classes are the following:

1. *Kalman systems* are first-order linear (ordinary) differential systems

$$\dot{x} = Ax + Bu, \quad y = Cx + Du,$$

where A , B , C , and D are matrices with real entries [5]. For example, RLC circuits can be described by Kalman systems.

2. *Polynomial systems* are higher-order differential systems expressed without the help of any state variable, in the form

$$(1) \quad P(d/dt)y(t) + Q(d/dt)u(t) = 0.$$

Here P and Q are matrices with coefficients that are scalar linear differential operators with real coefficients [5]. For example, a harmonic oscillator commanded by a force is described by a second-order polynomial system. By Laplace transform, an equivalent formulation of (1) is

$$P(s)\hat{y}(s) + Q(s)\hat{u}(s) = 0;$$

the matrices P and Q are now matrices of polynomials in s with real coefficients [5].

3. *Differential-delay systems with constant delays* are a generalization common to Kalman systems and polynomial systems by introducing the constant-delay operators δ_i defined by

$(\delta_i f)(t) = f(t - t_i)$ for some real t_i . The generalized forms are

$$\dot{x}(t) = \sum_{i=0}^r A_i x(t - t_i) + B_i u(t - t_i), \quad y(t) = \sum_{i=0}^r C_i x(t - t_i) + D_i u(t - t_i),$$

and

$$P(d/dt, \delta_1, \dots, \delta_r)y + Q(d/dt, \delta_1, \dots, \delta_r)u = 0,$$

respectively. A typical occurrence of delay is when transmitting a signal u through a channel.

4. *Multivariate linear differential systems with real coefficients* appear frequently to describe physical phenomena, like electromagnetism, (linear) elasticity, hydrodynamism, and so on [7, 8, 12].

In each case, the column vector $\xi = (y, x, u)^T$ satisfies $R\xi = 0$ for a (rectangular) matrix R with coefficients in some ring \mathbb{A} . Thus, we henceforth consider a linear control system as defined by a matrix R with coefficients in an entire ring \mathbb{A} . To give simple examples, the matrix forms corresponding to Kalman and polynomial systems respectively are

$$R = \begin{pmatrix} 0 & A - d/dt \text{Id} & B \\ \text{Id} & C & D \end{pmatrix} \quad \text{and} \quad R = \begin{pmatrix} P & Q \end{pmatrix}.$$

In these differential cases, the ring \mathbb{A} is $\mathbb{R}[d/dt]$ or a multivariate generalization, but more general rings of coefficients are also considered in place of \mathbb{R} in applications, like the ring $\mathbb{R}(t)$ of rational function, or the ring $C^\infty(I)$ of infinitely differentiable functions over some real interval I . In the equivalent formulation by Laplace transform or in the mixed differential-delay situation with *constant* coefficients, the ring is isomorphic to the polynomial ring $\mathbb{R}[s]$ or a multivariate analogue. Here again, more general rings of functions often appear in applications, like: $\mathbb{R}[s, \exp(-s)]$, for situations related to the wave equation; or the ring $H_\infty(\mathbb{C}_+)$ of complex-analytic functions bounded in the right half complex plane \mathbb{C}_+ (Hardy space) and its subring $\text{RH}_\infty(\mathbb{C}_+)$ of real rational functions with no pole on the right half complex plane, for the study of the stability of some distributed systems [11].

Several structural properties of systems are all-important in control theory. An *observable* of a control system is any scalar function of its command u , state x , and output y and of their derivatives up to a certain order. An observable is called *autonomous* if it satisfies a non-trivial PDE. A control system is called *controllable* if no observable is autonomous. The study of structural properties of a system turns out to lead to linear algebra: controllability and observability are related to various notions of primeness of the linear maps

$$z \mapsto Rz \quad \text{and} \quad z \mapsto zR;$$

in the polynomial systems case, stability is related to poles and zeroes of the system, that are invariant factors of the matrix R ; similarly with the existence of generalized Bézout identities and flatness of a control system; etc.

By associating an A -module M to the matrix R , another interpretation of the structural properties is in terms of module-theoretic and homological properties of M (torsion, torsion-free, reflexive, and projective modules; extension and torsion functors). In fact, a full classification of modules by homological algebra methods translates into a classification of linear control systems.

2. Duality Between Differential Operators and D-Modules

Let us turn to the formal theory of PDEs [13]. Starting with a naive viewpoint on differential operators (so as to avoid the formalism of jet bundles), we introduce *formally exact sequences of differential operators*. For each k , let F^k denote the algebra of functions in k variables, and consider

a differential operator \mathcal{D} from F^m to F^l (of finite order). Given $\eta \in F^n$, the necessary conditions for the existence of $\xi \in F^m$ such that $\mathcal{D}\xi = \eta$ are called *compatibility conditions* of \mathcal{D} ; they take the form $\mathcal{D}_1\eta = 0$ for some differential operator \mathcal{D}_1 . Writing $\mathcal{D}_0 = \mathcal{D}$, we have $\mathcal{D}_1 \circ \mathcal{D}_0 = 0$. When \mathcal{D}_1 encapsulates all compatibility conditions, the sequence

$$F^m \xrightarrow{\mathcal{D}_0} F^{l_0} \xrightarrow{\mathcal{D}_1} F^{l_1}$$

of differential operators is called *formally exact* (at F_{l_0}). Formally exact sequences can always be extended (to the right) into longer sequences, so that denoting the solution set of $\mathcal{D} = \mathcal{D}_0$ in F^m by Θ , we obtain a formally exact sequence

$$0 \rightarrow \Theta \rightarrow F^m \xrightarrow{\mathcal{D}_0} F^{l_0} \xrightarrow{\mathcal{D}_1} F^{l_1} \xrightarrow{\mathcal{D}_2} F^{l_2} \rightarrow \dots$$

(at Θ and each F^{l_k}) where the first two maps denote inclusions. Under technical conditions (*regularity* and *involutivity*), the formal theory of PDEs proves the existence of a *finite* formally exact sequence for \mathcal{D} , in the sense that $F^{l_n} = 0$ from some n on, by exhibiting a canonical, formally exact sequence

$$(2) \quad 0 \rightarrow \Theta = \ker \mathcal{D}_0 \rightarrow F^m \xrightarrow{\mathcal{D}_0} F^{l_0} \xrightarrow{\mathcal{D}_1} F^{l_1} \xrightarrow{\mathcal{D}_2} F^{l_2} \rightarrow \dots \xrightarrow{\mathcal{D}_r} F^{l_r} \rightarrow 0$$

called the *Janet sequence* of \mathcal{D} , in which each (non-zero) \mathcal{D}_i is of order 1 (and involutive) for $i \geq 1$, and r is the number of derivatives.

A dual, more algebraic counterpart to this differential viewpoint is in terms of *exact sequences of D -modules*. To this end, we now view each \mathcal{D}_i as defined by an $l_i \times l_{i-1}$ matrix R_i of multivariate linear differential operators in

$$\mathbb{A} = \mathbb{R}(x_1, \dots, x_r)[\partial_1, \dots, \partial_r].$$

(We set $l_{-1} = m$.) In terms of matrices,

$$\mathcal{D}_i = R_i \cdot = (\xi \mapsto R_i \xi),$$

so that $R_{i+1}R_i \cdot = 0$. We then consider the maps $\cdot R_i$ from \mathbb{A}^{l_i} to $\mathbb{A}^{l_{i-1}}$, whose elements are viewed as row vectors. To start with, the map $\cdot R_0$ defines an algebraic representation of a generic solution ξ the PDE system $\mathcal{D}_0\xi = 0$ in the following way. Let (e_1, \dots, e_m) be the canonical basis of \mathbb{A}^m and consider the maps

$$(3) \quad 0 \leftarrow M = \mathbb{A}^m / \mathbb{A}^{l_0} R_0 \xleftarrow{\pi} \mathbb{A}^m \xleftarrow{\cdot R_0} \mathbb{A}^{l_0},$$

where π denotes the canonical projection $\pi(v) = v + \mathbb{A}^{l_0} R_0$. The *cokernel*

$$M = \text{coker}(\cdot R_0) = \mathbb{A}^m / \mathbb{A}^{l_0} R_0$$

of $\cdot R_0$ contains the announced generic solution: setting

$$\xi_i = \pi(e_i) = e_i + \mathbb{A}^{l_0} R_0,$$

we get $\mathcal{D}_0\xi = \xi R_0 = 0$. Other members of M correspond to linear combinations of the ξ_i and their derivatives, i.e., to the observables defined above. We now proceed to follow up with the next \mathcal{D}_i 's. A sequence

$$L \xrightarrow{u} L' \xrightarrow{v} L''$$

of linear maps (between modules) is said to be *exact* (at L') if $\text{im } u = \ker v$. (Thus (3) is exact at M and \mathbb{A}_{l_0} .) It can be shown that any Janet sequence (2) gives rise to the exact sequence

$$(4) \quad 0 \leftarrow M \xleftarrow{\pi} \mathbb{A}^m \xleftarrow{\cdot R_0} \mathbb{A}^{l_0} \xleftarrow{\cdot R_1} \mathbb{A}^{l_1} \xleftarrow{\cdot R_2} \mathbb{A}^{l_2} \leftarrow \dots \xleftarrow{\cdot R_r} \mathbb{A}^{l_r} \leftarrow 0$$

(at M and each \mathbb{A}^{l_k}). Here, $\cdot R_{i+1}R_i = 0$ by exactness. Since \mathbb{A} has no zero divisor, this means that $R_{i+1}R_i = 0$. The sequence (4) of (left) \mathcal{D} -modules is called a *free resolution* of M : it encapsulates the obstruction of M to be free (as the module $\ker \pi = \text{im}(\cdot R_0)$), then the obstruction of $\ker \pi$ to be free (as the module $\ker(\cdot R_0) = \text{im}(\cdot R_1)$), etc. (A module is called *free* when it is isomorphic to some \mathbb{A}^r , whence the name “free resolution.”)

3. Parametrization and Controllability

A problem dual to the search of compatibility conditions is, for a given differential equation $\mathcal{D}\xi = 0$, to determine whether the solutions can be parametrized by certain arbitrary functions which, in physical systems, play the role of *potentials*. In other words, the problem is to determine whether there exists another operator

$$\mathcal{D}_{-1} : F^{l-1} \rightarrow F^{l_0}$$

whose compatibility conditions are described by $\mathcal{D} = \mathcal{D}_0$, i.e., to look for a formally exact sequence

$$F^{l-1} \xrightarrow{\mathcal{D}_{-1}} F^{l_0} \xrightarrow{\mathcal{D}_0} F^{l_1}.$$

In this situation, for any $\xi \in F^{l_0}$ the existence of $\pi \in F^{l-1}$ satisfying $\mathcal{D}_{-1}\pi = \xi$ is equivalent to the fact that ξ solves the differential equation $\mathcal{D}_0\xi = 0$, and so \mathcal{D}_{-1} “parametrizes”—in the usual sense—all its solutions.

The existence of a parametrization has a nice application to *optimal command*: assume one needs to minimize a cost function provided by the integral $\int_0^T F(t) dt$ of an observable F of some system \mathcal{D}_0 . The optimization problem is then to minimize over all tuples $\xi = (y, x, u)^T$ of functions constrained by $\mathcal{D}_0\xi = 0$. On the other hand, once the solutions ξ are given by a parametrization $\xi = \mathcal{D}_{-1}\pi$, the optimization problem reduces to the non-constrained problem of minimizing the integral $\int_0^T G(t) dt$ of a new observable G of \mathcal{D}_{-1} over unconstrained π [12].

To study the control-theoretic properties of the differential operator \mathcal{D} , starting with the existence of a parametrization, we in fact study the module-theoretic properties of M , which in turn are derived from the study of the right \mathcal{D} -module defined by

$$(5) \quad \mathbb{A}^{l-1} \xrightarrow{R_0} \mathbb{A}^{l_0} \rightarrow N = \text{coker}(R_0 \cdot) = \mathbb{A}^{l_0} / R_0 \mathbb{A}^{l-1} \rightarrow 0$$

(recall that $l_{-1} = m$ and compare with (3)). The key ingredient to be used comes from linear algebra: dualization, which maps a left \mathbb{A} -module L to the right module $\text{hom}_{\mathbb{A}}(L, \mathbb{A})$ of \mathbb{A} -linear applications from L to \mathbb{A} . Correspondingly, any linear map $L \xrightarrow{u} L'$ induces a map from the dual of L' to the dual of L : to $\lambda \in \text{hom}_{\mathbb{A}}(L', \mathbb{A})$, one associates $\lambda \circ u \in \text{hom}_{\mathbb{A}}(L, \mathbb{A})$. This takes a simple form when the modules are free and of finite rank (i.e., $L = \mathbb{A}^m$ and $L' = \mathbb{A}^l$, viewed as left modules of row vectors). Indeed, the linear map u is just the application of an $m \times l$ matrix U : $u = \cdot U$. Elements $\mu \in \text{hom}_{\mathbb{A}}(\mathbb{A}^k, \mathbb{A})$ are defined by their values on the canonical basis (e_i) of \mathbb{A}^k by

$$\mu = \cdot (\mu(e_1), \dots, \mu(e_k))^T,$$

so that the dual of \mathbb{A}^k is isomorphic to \mathbb{A}^k (now viewed as a right module of column vectors). In this setting, the dual of a map $\mathbb{A}^m \xrightarrow{U} \mathbb{A}^l$ is $\mathbb{A}^m \xleftarrow{U} \mathbb{A}^l$. The same ideas apply mutatis mutandis for the dual of right modules.

To search for a parametrization, one thus extends the exact sequence (5) into an exact sequence

$$\mathbb{A}^{l-2} \xrightarrow{R_{-1}} \mathbb{A}^{l-1} \xrightarrow{R_0} \mathbb{A}^{l_0} \rightarrow N \rightarrow 0.$$

An algorithm for this purpose will be given in Section 5. By dualization (i.e., application of the $\text{hom}_{\mathbb{A}}(\cdot, \mathbb{A})$ functor), it becomes a sequence

$$\mathbb{A}^{l-2} \xleftarrow{\cdot R_{-1}} \mathbb{A}^{l-1} \xleftarrow{\cdot R_0} \mathbb{A}^{l_0} \leftarrow \text{hom}_{\mathbb{A}}(N, \mathbb{A}) \leftarrow 0$$

of left D-modules that is *usually no longer exact*. In particular, we may well have $\ker(\cdot R_{-1})$ strictly larger than $\text{im}(\cdot R_0)$. Upon forgetting the map $\cdot R_0$ and prolonging $\cdot R_{-1}$ into

$$\mathbb{A}^{l-2} \xleftarrow{\cdot R_{-1}} \mathbb{A}^{l-1} \xleftarrow{\cdot R'_0} \mathbb{A}'_0,$$

we obtain an “exact” representation of $\ker(\cdot R_{-1})$ as $\text{im}(\cdot R'_0)$. It can be proved that the quotient

$$\text{im}(\cdot R'_0) / \text{im}(\cdot R_0) \subseteq M$$

is the *torsion module* $t(M)$ of M , i.e., the set of all its members m for which there exists a non-zero scalar $a \in \mathbb{A}$ such that $am = 0$. Thus we have obtained that a (linear) control system is controllable if and only if its associated module M of observables is torsion-free, which can be tested algorithmically. Moreover, a basis for the module $t(M)$ of autonomous elements is obtained from the rows of R'_0 (that are elements of $\text{im}(\cdot R'_0)$), viewed modulo $\text{im}(\cdot R_0)$.

4. More Structural Properties of Control Systems as Extension Modules

Other structural properties of \mathcal{D} will be described in terms of the *extension modules* of N , a central tool in homological algebra. Consider a free resolution

$$(6) \quad \dots \xrightarrow{R_{-n}} \mathbb{A}^{l-n} \xrightarrow{R_{-n+1}} \dots \xrightarrow{R_{-2}} \mathbb{A}^{l-2} \xrightarrow{R_{-1}} \mathbb{A}^{l-1} \xrightarrow{R_0} \mathbb{A}^{l_0} \rightarrow N \rightarrow 0$$

(as obtained, for example, with the algorithms of Section 5). This is an exact sequence of right D-modules. By dualization it becomes a sequence

$$(7) \quad \dots \xleftarrow{\cdot R_{-n}} \mathbb{A}^{l-n} \xleftarrow{\cdot R_{-n+1}} \dots \xleftarrow{\cdot R_{-2}} \mathbb{A}^{l-2} \xleftarrow{\cdot R_{-1}} \mathbb{A}^{l-1} \xleftarrow{\cdot R_0} \mathbb{A}^{l_0} \leftarrow \text{hom}_{\mathbb{A}}(N, \mathbb{A}) \leftarrow 0$$

of left D-modules that, again, is usually no longer exact. By dropping $\text{hom}_{\mathbb{A}}(N, \mathbb{A})$ from (7), we obtain another non-exact sequence, but of *free* modules only,

$$\dots \xleftarrow{\cdot R_{-n}} \mathbb{A}^{l-n} \xleftarrow{\cdot R_{-n+1}} \dots \xleftarrow{\cdot R_{-2}} \mathbb{A}^{l-2} \xleftarrow{\cdot R_{-1}} \mathbb{A}^{l-1} \xleftarrow{\cdot R_0} \mathbb{A}^{l_0} \leftarrow 0.$$

Its defects of exactness are encapsulated by its *cohomology* sequence, that is to say, by the quotients

$$\ker(\cdot R_{-i}) / \text{im}(\cdot R_{-i+1}).$$

An all-important fact is that this family depends on N only, and not of the choice of a free resolution (6). This motivates the notation

$$\text{ext}_{\mathbb{A}}^i(N, \mathbb{A}) = \ker(\cdot R_{-i}) / \text{im}(\cdot R_{-i+1})$$

for extension modules (with in particular $\text{ext}_{\mathbb{A}}^0(N, \mathbb{A}) = \ker(\cdot R_0) = \text{hom}_{\mathbb{A}}(N, \mathbb{A})$).

The nullity or non-nullity of the ext^i 's provides with the classification of modules in Theorem 1 below; in turn this classification provides with the classification of control systems in Theorem 3 below. Here are two more module-theoretic notions missing to state Theorem 1. A module L is *projective* whenever there exists a module L' such that $L \oplus L'$ is free; it is *reflexive* whenever it is isomorphic to the dual of its dual through the linear map

$$\epsilon : M \rightarrow \text{hom}_{\mathbb{A}}(\text{hom}_{\mathbb{A}}(M, \mathbb{A}), \mathbb{A})$$

defined by

$$\epsilon(m)(f) = f(m).$$

Then, a free module is always projective, a projective module always reflexive, and a reflexive module always torsion-free. (For modules over a principal ideal, these notions coincide; for modules over a multivariate polynomial ring with coefficients over a field, free and projective are equivalent, a theorem by Quillen and Suslin.)

The following theorems [1, 4] make the link between properties of a module and the nullity of the extension modules of its transposed module.

Theorem 1 (Palamodov, Kashiwara). *For the modules M and N defined by (3) and (5), we have:*

1. M is torsion-free if and only if $\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = 0$;
2. M is reflexive if and only if $\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = \text{ext}_{\mathbb{A}}^2(N, \mathbb{A}) = 0$;
3. M is projective if and only if $\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = \dots = \text{ext}_{\mathbb{A}}^r(N, \mathbb{A}) = 0$.

Theorem 2 (Palamodov, Kashiwara). *Let M and N be the two modules defined by (3) and (5). Then there exists an exact sequence*

$$0 \rightarrow M \rightarrow \mathbb{A}^{p_1} \rightarrow \mathbb{A}^{p_2} \rightarrow \dots \rightarrow \mathbb{A}^{p_r}$$

if and only if $\text{ext}_{\mathbb{A}}^i(N, \mathbb{A}) = 0$ for $i = 1, \dots, r$.

We finally obtain the following classification of linear control systems, which admits some refinements in the case of differential operators with constant coefficients, i.e., matrices with entries in $\mathbb{R}[\partial_1, \dots, \partial_r] \subset \mathbb{A}$ [7, 8, 12].

Theorem 3. *For a control system defined by the differential operator $\mathcal{D} = R \cdot$ where R is an $l \times m$ matrix with $l \leq m$ and entries in*

$$\mathbb{A} = \mathbb{R}(x_1, \dots, x_r)[\partial_1, \dots, \partial_r],$$

introduce the two left D -modules $M = \text{coker}(\cdot R)$ and $N = \text{coker}(R \cdot)$ of the maps between the free modules \mathbb{A}^m and \mathbb{A}^l . Then:

1. *if M has torsion, the control system has autonomous elements, and in the event R has constant coefficients and full row module, it has no primality property;*
2. *M is torsion-free if and only if $\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = 0$. In this case, the control system is controllable, and in the event R has constant coefficients and full row module, it is prime in the sense of minors, i.e., there is no common factor between the minors of R of order l ;*
3. *M is reflexive if and only if $\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = \text{ext}_{\mathbb{A}}^2(N, \mathbb{A}) = 0$;*
4. *in the event R has constant coefficients and full row module, and if*

$$\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = \dots = \text{ext}_{\mathbb{A}}^{r-1}(N, \mathbb{A}) = 0 \quad \text{while} \quad \text{ext}_{\mathbb{A}}^r(N, \mathbb{A}) \neq 0,$$

the control system is weakly prime in the sense of zeroes, i.e., all minors of order l simultaneously vanish at finitely many points only;

5. *M is projective if and only if*

$$\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = \dots = \text{ext}_{\mathbb{A}}^r(N, \mathbb{A}) = 0.$$

In this case the control system has an inverse generalized Bézout identity, and in the event R has constant coefficients and full row module, it is prime in the sense of zeroes, i.e., all minors of order l simultaneously vanish at no point;

6. *if M is free, the control system is flat and has direct and inverse generalized Bézout identities.*

Further intermediate situations, $\text{ext}_{\mathbb{A}}^1(N, \mathbb{A}) = \dots = \text{ext}_{\mathbb{A}}^{k-1}(N, \mathbb{A}) = 0$ and $\text{ext}_{\mathbb{A}}^k(N, \mathbb{A}) \neq 0$, correspond to further intermediate primeness conditions (described in terms of the dimension of the algebraic variety defined by the $l \times l$ minors of R).

5. Gröbner Basis Calculations for Compatibility Conditions and Parametrizations

The whole machinery of the previous sections crucially bases on prolongations of exact sequences. A point that is important in view of computations is that these can be obtained by Gröbner basis calculations for free modules over \mathbb{A} .

The prolongation of a map $\mathbb{A}^m \xleftarrow{R} \mathbb{A}^l$ into an exact sequence $\mathbb{A}^m \xleftarrow{R} \mathbb{A}^l \xleftarrow{S} \mathbb{A}^k$ is done in the following fashion. Let (e_1, \dots, e_m) and (f_1, \dots, f_l) be the canonical bases of \mathbb{A}^m and \mathbb{A}^l , respectively, and denote the i th row of $R = (r_{i,j})$ by η_i . Thus $\eta_i = \sum_{j=1}^m r_{i,j} e_j$. Prolonging the map amounts to finding non-trivial relations $\sum_{i=1}^l s_i \eta_i = 0$. Now introduce the submodule Z of \mathbb{A}^{m+l} generated by the formal linear combinations $f_i - \eta_i$. We contend that computing a Gröbner basis for this module and for a term order that *eliminates* the e_i results in linear combinations $\sum_{i=1}^l s_i f_i \in Z$, each of which corresponds to a relation between the η_i . Additionally, any relation can be obtained as a linear combination of the relations thus obtained.

In effect, consider an element $z = \sum_{i=1}^l s_i f_i \in Z$; thus $\sum_{i=1}^l s_i \eta_i$ is in Z and is a combination $\sum_{i=1}^l \lambda_i (f_i - \eta_i)$, which is only possible, in view of the coefficients of the f_i , if the λ_i are zero, thus if $\sum_{i=1}^l s_i \eta_i = 0$; the converse property is also true. Since the Gröbner basis calculation precisely computes a finite generating set, say of k elements, for all the z 's free of the e_i , it suffices to consider each of those k elements as a row, and to glue them in column to obtain a new matrix $S = (S_{i,j})$ such that the sequence $\mathbb{A}^m \xleftarrow{R} \mathbb{A}^l \xleftarrow{S} \mathbb{A}^k$ is exact.

Now, existing packages often contain facilities to compute Gröbner bases for left modules only; some of our computations require to deal with right modules. A last ingredient, *adjunction*, enables one to turn any left module into a right module, and vice versa, in a way *that preserves the exactness of sequences*. Indeed, the adjoint map $P \mapsto \tilde{P}$ defined by associativity from the rules $\tilde{x}_i = x_i$, $\tilde{\partial}_i = -\partial_i$, and $(PQ)^\sim = \tilde{Q}\tilde{P}$, is an (anti)automorphism of the algebra \mathbb{A} which extends to matrices by mapping itself to the entries of the transpose matrix. Thus, for example, the exact sequence (5) of right D-modules of columns in Section 3 is replaced with the exact sequence

$$\mathbb{A}^{l-1} \xrightarrow{\tilde{R}_0} \mathbb{A}^{l_0} \rightarrow \tilde{N} = \text{coker}(\cdot \tilde{R}_0) \rightarrow 0$$

of left D-modules of lines, for the purpose of explicit calculations.

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